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Norbornane-2,7-diyl 1',2'-phenylene orthocarbonate

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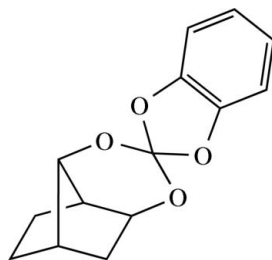
Received 28 August 2007; accepted 29 August 2007

Key indicators: single-crystal X-ray study; $T = 200$ K; mean $\sigma(\text{C}-\text{C}) = 0.002$ Å; R factor = 0.044; wR factor = 0.117; data-to-parameter ratio = 15.7.

In the title compound, $\text{C}_{14}\text{H}_{14}\text{O}_4$, which was synthesized in order to compare its NMR spectroscopic data with those of similar silicon compounds, the incorporation of chelating hydroxyl groups into the parent rigid bicyclic framework ensures that the resulting six-membered chelate ring has a boat conformation.

Related literature

For synthesis, see Mues & Buysch (1990).



Experimental

Crystal data

$\text{C}_{14}\text{H}_{14}\text{O}_4$
 $M_r = 246.26$

Monoclinic, $P2_1/n$
 $a = 6.0509$ (2) Å

$b = 18.1250$ (6) Å
 $c = 10.3711$ (3) Å
 $\beta = 95.689$ (2)°
 $V = 1131.82$ (6) Å³
 $Z = 4$

Mo $K\alpha$ radiation
 $\mu = 0.11$ mm⁻¹
 $T = 200$ (2) K
 $0.16 \times 0.15 \times 0.10$ mm

Data collection

Nonius KappaCCD diffractometer
Absorption correction: none
5009 measured reflections

2573 independent reflections
1779 reflections with $I > 2\sigma(I)$
 $R_{\text{int}} = 0.028$

Refinement

$R[F^2 > 2\sigma(F^2)] = 0.044$
 $wR(F^2) = 0.117$
 $S = 1.03$
2573 reflections
164 parameters

Only H-atom displacement parameters refined
 $\Delta\rho_{\text{max}} = 0.19$ e Å⁻³
 $\Delta\rho_{\text{min}} = -0.20$ e Å⁻³

Table 1

Selected bond lengths (Å).

| | | | |
|---------|-----------|---------|-----------|
| O12—C10 | 1.364 (2) | O21—C10 | 1.413 (2) |
| O17—C10 | 1.369 (2) | O22—C10 | 1.451 (2) |

Data collection: *COLLECT* (Nonius, 2004); cell refinement: *SCALEPACK* (Otwinowski & Minor, 1997); data reduction: *SCALEPACK* and *DENZO* (Otwinowski & Minor, 1997); program(s) used to solve structure: *SHELXS97* (Sheldrick, 1997); program(s) used to refine structure: *SHELXL97* (Sheldrick, 1997); molecular graphics: *ORTEPIII* (Burnett & Johnson, 1996); software used to prepare material for publication: *SHELXL97*.

The authors thank Sandra Albrecht for professional support.

Supplementary data and figures for this paper are available from the IUCr electronic archives (Reference: NG2315).

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Mues, P. & Buysch, H.-J. (1990). *Synthesis*, pp. 249–252.
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Sheldrick, G. M. (1997). *SHELXS97* and *SHELXL97*. University of Göttingen, Germany.

supplementary materials

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Norbornane-2,7-diyl 1',2'-phenylene orthocarbonate

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Comment

The title compound, C₁₄H₁₄O₄, was prepared for the purpose of collecting NMR data on orthocarbonates and for comparison with similar silicon compounds. The incorporation of the chelating hydroxyl groups into the rigid bicyclic framework ensures the six-membered chelate ring to be present in a boat conformation. The markedly large range of the C—O distances at the spiro center is in agreement with a DFT calculation on a single molecule, i. e., it is not indicative of special packing forces in the crystalline state.

The molecular structure (Fig. 1) shows a norbornane-2,7-dioxy and a benzene-1,2-dioxy fragment attached to a carbon atom.

The molecular packing is shown in Figure 2.

Experimental

The title compound was prepared according to standard procedures (Mues & Buysch, 1990) upon reaction of 2,2-dichlorobenzo[1.3]dioxole with 2,7-norbornanediol in the presence of pyridine in dichloromethane. Crystals suitable for X-ray analysis were directly obtained from the recrystallized reaction product.

Refinement

All H atoms were located in a difference map and refined as riding on their parent atoms. One common isotropic displacement parameter for all H atoms was refined to $U_{\text{iso}}(\text{H}) = 0.0463$ (14).

Figures

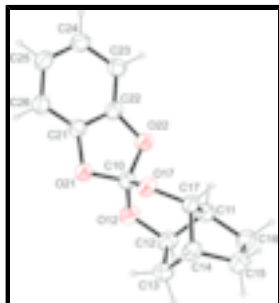


Fig. 1. The molecular of (I). Anisotropic displacement ellipsoids are drawn at the 50%-probability level for non-H atoms.

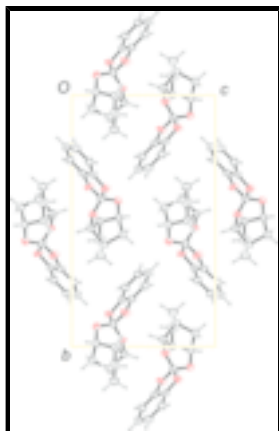


Fig. 2. The packing of (I) viewed along [1 0 0].

Norbornane-2,7-diyl 1',2'-phenylene orthocarbonate

Crystal data

$C_{14}H_{14}O_4$

$M_r = 246.26$

Monoclinic, $P2_1/n$

Hall symbol: $-P\ 2_1n$

$a = 6.0509\ (2)\ \text{\AA}$

$b = 18.1250\ (6)\ \text{\AA}$

$c = 10.3711\ (3)\ \text{\AA}$

$\beta = 95.689\ (2)^\circ$

$V = 1131.82\ (6)\ \text{\AA}^3$

$Z = 4$

$F_{000} = 520$

$D_x = 1.445\ \text{Mg m}^{-3}$

Mo $K\alpha$ radiation

$\lambda = 0.71073\ \text{\AA}$

Cell parameters from 11723 reflections

$\theta = 3.1\text{--}27.5^\circ$

$\mu = 0.11\ \text{mm}^{-1}$

$T = 200\ (2)\ \text{K}$

Block, colourless

$0.16 \times 0.15 \times 0.10\ \text{mm}$

Data collection

Nonius KappaCCD
diffractometer

Radiation source: rotating anode

Monochromator: MONTEL, graded multilayered X-ray optics

$T = 200\ (2)\ \text{K}$

CCD; rotation images; thick slices scans

Absorption correction: none

5009 measured reflections

2573 independent reflections

1779 reflections with $I > 2\sigma(I)$

$R_{\text{int}} = 0.028$

$\theta_{\text{max}} = 27.5^\circ$

$\theta_{\text{min}} = 3.6^\circ$

$h = -7 \rightarrow 7$

$k = -23 \rightarrow 23$

$l = -13 \rightarrow 13$

Refinement

Refinement on F^2

Least-squares matrix: full

$R[F^2 > 2\sigma(F^2)] = 0.044$

Secondary atom site location: difference Fourier map

Hydrogen site location: difference Fourier map

Only H-atom displacement parameters refined

| | |
|--|--|
| $wR(F^2) = 0.117$ | $w = 1/[\sigma^2(F_o^2) + (0.0525P)^2]$ |
| $S = 1.03$ | where $P = (F_o^2 + 2F_c^2)/3$ |
| 2573 reflections | $(\Delta/\sigma)_{\max} < 0.001$ |
| 164 parameters | $\Delta\rho_{\max} = 0.19 \text{ e } \text{\AA}^{-3}$ |
| Primary atom site location: structure-invariant direct methods | $\Delta\rho_{\min} = -0.20 \text{ e } \text{\AA}^{-3}$ |
| | Extinction correction: none |

Special details

Geometry. All e.s.d.'s (except the e.s.d. in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell e.s.d.'s are taken into account individually in the estimation of e.s.d.'s in distances, angles and torsion angles; correlations between e.s.d.'s in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell e.s.d.'s is used for estimating e.s.d.'s involving l.s. planes.

Refinement. Refinement of F^2 against ALL reflections. The weighted R -factor wR and goodness of fit S are based on F^2 , conventional R -factors R are based on F , with F set to zero for negative F^2 . The threshold expression of $F^2 > 2\text{sigma}(F^2)$ is used only for calculating R -factors(gt) *etc.* and is not relevant to the choice of reflections for refinement. R -factors based on F^2 are statistically about twice as large as those based on F , and R -factors based on ALL data will be even larger.

Fractional atomic coordinates and isotropic or equivalent isotropic displacement parameters (\AA^2)

| | x | y | z | $U_{\text{iso}}^*/U_{\text{eq}}$ |
|------|--------------|---------------|--------------|----------------------------------|
| O12 | 0.83506 (19) | 0.08057 (6) | 0.82385 (11) | 0.0373 (3) |
| O17 | 0.97730 (18) | 0.02608 (6) | 0.64946 (11) | 0.0327 (3) |
| O21 | 1.13089 (19) | 0.12882 (6) | 0.73797 (11) | 0.0377 (3) |
| O22 | 0.78699 (19) | 0.13656 (6) | 0.62400 (11) | 0.0382 (3) |
| C10 | 0.9290 (3) | 0.09008 (9) | 0.71081 (16) | 0.0320 (4) |
| C11 | 0.5901 (3) | -0.00278 (9) | 0.69471 (17) | 0.0350 (4) |
| H11 | 0.5102 | 0.0399 | 0.6503 | 0.0463 (14)* |
| C12 | 0.7030 (3) | 0.01341 (9) | 0.82865 (16) | 0.0358 (4) |
| H12 | 0.5917 | 0.0181 | 0.8934 | 0.0463 (14)* |
| C13 | 0.8536 (3) | -0.05454 (9) | 0.85779 (16) | 0.0393 (4) |
| H131 | 1.0068 | -0.0395 | 0.8894 | 0.0463 (14)* |
| H132 | 0.7944 | -0.0870 | 0.9230 | 0.0463 (14)* |
| C14 | 0.8472 (3) | -0.09294 (9) | 0.72612 (17) | 0.0359 (4) |
| H14 | 0.9839 | -0.1216 | 0.7118 | 0.0463 (14)* |
| C15 | 0.6297 (3) | -0.13617 (10) | 0.70228 (19) | 0.0415 (4) |
| H151 | 0.6115 | -0.1711 | 0.7739 | 0.0463 (14)* |
| H152 | 0.6220 | -0.1637 | 0.6195 | 0.0463 (14)* |
| C16 | 0.4545 (3) | -0.07430 (10) | 0.69715 (19) | 0.0427 (4) |
| H161 | 0.3488 | -0.0787 | 0.6183 | 0.0463 (14)* |
| H162 | 0.3706 | -0.0759 | 0.7743 | 0.0463 (14)* |
| C17 | 0.7989 (3) | -0.02808 (9) | 0.63485 (16) | 0.0324 (4) |
| H17 | 0.7652 | -0.0443 | 0.5428 | 0.0463 (14)* |
| C21 | 1.1277 (3) | 0.18638 (8) | 0.64979 (15) | 0.0316 (4) |
| C22 | 0.9223 (3) | 0.19053 (8) | 0.58122 (15) | 0.0317 (4) |
| C23 | 0.8708 (3) | 0.24313 (9) | 0.48849 (16) | 0.0370 (4) |

supplementary materials

| | | | | |
|-----|------------|-------------|--------------|--------------|
| H23 | 0.7282 | 0.2457 | 0.4413 | 0.0463 (14)* |
| C24 | 1.0393 (3) | 0.29288 (9) | 0.46697 (16) | 0.0389 (4) |
| H24 | 1.0114 | 0.3303 | 0.4034 | 0.0463 (14)* |
| C25 | 1.2457 (3) | 0.28872 (9) | 0.53632 (17) | 0.0391 (4) |
| H25 | 1.3565 | 0.3235 | 0.5194 | 0.0463 (14)* |
| C26 | 1.2961 (3) | 0.23468 (9) | 0.63083 (16) | 0.0365 (4) |
| H26 | 1.4378 | 0.2316 | 0.6789 | 0.0463 (14)* |

Atomic displacement parameters (\AA^2)

| | U^{11} | U^{22} | U^{33} | U^{12} | U^{13} | U^{23} |
|-----|-------------|-------------|-------------|-------------|-------------|-------------|
| O12 | 0.0485 (7) | 0.0298 (6) | 0.0347 (6) | -0.0033 (5) | 0.0092 (5) | -0.0051 (5) |
| O17 | 0.0337 (6) | 0.0282 (6) | 0.0374 (6) | -0.0027 (5) | 0.0089 (5) | -0.0021 (5) |
| O21 | 0.0360 (7) | 0.0316 (6) | 0.0436 (7) | -0.0057 (5) | -0.0059 (5) | 0.0068 (5) |
| O22 | 0.0330 (6) | 0.0328 (6) | 0.0476 (7) | -0.0042 (5) | -0.0030 (5) | 0.0084 (5) |
| C10 | 0.0333 (9) | 0.0272 (8) | 0.0346 (8) | -0.0008 (7) | -0.0005 (7) | 0.0016 (7) |
| C11 | 0.0299 (9) | 0.0331 (9) | 0.0419 (9) | 0.0010 (7) | 0.0025 (7) | 0.0050 (7) |
| C12 | 0.0425 (10) | 0.0318 (9) | 0.0354 (9) | -0.0015 (7) | 0.0143 (8) | -0.0020 (7) |
| C13 | 0.0448 (11) | 0.0357 (9) | 0.0364 (9) | -0.0001 (8) | -0.0009 (8) | 0.0059 (7) |
| C14 | 0.0353 (9) | 0.0290 (8) | 0.0443 (9) | 0.0015 (7) | 0.0075 (8) | -0.0007 (7) |
| C15 | 0.0427 (10) | 0.0348 (9) | 0.0475 (10) | -0.0067 (8) | 0.0066 (8) | -0.0010 (8) |
| C16 | 0.0337 (10) | 0.0438 (10) | 0.0506 (11) | -0.0060 (8) | 0.0043 (8) | 0.0033 (8) |
| C17 | 0.0349 (9) | 0.0306 (8) | 0.0323 (8) | -0.0070 (7) | 0.0066 (7) | -0.0031 (7) |
| C21 | 0.0376 (9) | 0.0241 (8) | 0.0328 (8) | -0.0006 (7) | 0.0024 (7) | -0.0002 (6) |
| C22 | 0.0351 (9) | 0.0246 (8) | 0.0356 (8) | -0.0035 (7) | 0.0042 (7) | -0.0013 (6) |
| C23 | 0.0407 (10) | 0.0318 (9) | 0.0369 (9) | -0.0008 (7) | -0.0038 (8) | 0.0012 (7) |
| C24 | 0.0515 (11) | 0.0298 (9) | 0.0350 (9) | -0.0030 (8) | 0.0019 (8) | 0.0036 (7) |
| C25 | 0.0450 (11) | 0.0323 (9) | 0.0407 (9) | -0.0102 (8) | 0.0070 (8) | -0.0003 (7) |
| C26 | 0.0354 (9) | 0.0335 (9) | 0.0397 (9) | -0.0040 (7) | -0.0002 (7) | -0.0025 (7) |

Geometric parameters (\AA , $^\circ$)

| | | | |
|----------|-------------|----------|-----------|
| O12—C10 | 1.364 (2) | C14—C15 | 1.530 (2) |
| O12—C12 | 1.4598 (19) | C14—H14 | 1.0000 |
| O17—C10 | 1.3685 (19) | C15—C16 | 1.541 (2) |
| O17—C17 | 1.4557 (18) | C15—H151 | 0.9900 |
| O21—C21 | 1.3862 (19) | C15—H152 | 0.9900 |
| O21—C10 | 1.4129 (19) | C16—H161 | 0.9900 |
| O22—C22 | 1.3770 (18) | C16—H162 | 0.9900 |
| O22—C10 | 1.4510 (19) | C17—H17 | 1.0000 |
| C11—C12 | 1.515 (3) | C21—C22 | 1.371 (2) |
| C11—C17 | 1.532 (2) | C21—C26 | 1.372 (2) |
| C11—C16 | 1.536 (2) | C22—C23 | 1.368 (2) |
| C11—H11 | 1.0000 | C23—C24 | 1.395 (2) |
| C12—C13 | 1.544 (2) | C23—H23 | 0.9500 |
| C12—H12 | 1.0000 | C24—C25 | 1.380 (3) |
| C13—C14 | 1.530 (2) | C24—H24 | 0.9500 |
| C13—H131 | 0.9900 | C25—C26 | 1.398 (2) |
| C13—H132 | 0.9900 | C25—H25 | 0.9500 |

| | | | |
|-----------------|--------------|-----------------|--------------|
| C14—C17 | 1.519 (2) | C26—H26 | 0.9500 |
| C10—O12—C12 | 114.27 (12) | C14—C15—H151 | 111.3 |
| C10—O17—C17 | 115.45 (12) | C16—C15—H151 | 111.3 |
| C21—O21—C10 | 106.68 (12) | C14—C15—H152 | 111.3 |
| C22—O22—C10 | 106.13 (12) | C16—C15—H152 | 111.3 |
| O12—C10—O17 | 114.77 (13) | H151—C15—H152 | 109.2 |
| O12—C10—O21 | 108.50 (13) | C11—C16—C15 | 104.34 (13) |
| O17—C10—O21 | 107.08 (13) | C11—C16—H161 | 110.9 |
| O12—C10—O22 | 109.58 (13) | C15—C16—H161 | 110.9 |
| O17—C10—O22 | 110.14 (13) | C11—C16—H162 | 110.9 |
| O21—C10—O22 | 106.40 (12) | C15—C16—H162 | 110.9 |
| C12—C11—C17 | 96.58 (14) | H161—C16—H162 | 108.9 |
| C12—C11—C16 | 109.98 (14) | O17—C17—C14 | 111.23 (13) |
| C17—C11—C16 | 102.57 (13) | O17—C17—C11 | 112.88 (13) |
| C12—C11—H11 | 115.2 | C14—C17—C11 | 95.42 (12) |
| C17—C11—H11 | 115.2 | O17—C17—H17 | 112.1 |
| C16—C11—H11 | 115.2 | C14—C17—H17 | 112.1 |
| O12—C12—C11 | 109.20 (13) | C11—C17—H17 | 112.1 |
| O12—C12—C13 | 110.93 (14) | C22—C21—C26 | 122.57 (15) |
| C11—C12—C13 | 103.22 (13) | C22—C21—O21 | 109.65 (13) |
| O12—C12—H12 | 111.1 | C26—C21—O21 | 127.77 (15) |
| C11—C12—H12 | 111.1 | C23—C22—C21 | 122.30 (15) |
| C13—C12—H12 | 111.1 | C23—C22—O22 | 128.34 (15) |
| C14—C13—C12 | 103.05 (13) | C21—C22—O22 | 109.34 (14) |
| C14—C13—H131 | 111.2 | C22—C23—C24 | 116.35 (16) |
| C12—C13—H131 | 111.2 | C22—C23—H23 | 121.8 |
| C14—C13—H132 | 111.2 | C24—C23—H23 | 121.8 |
| C12—C13—H132 | 111.2 | C25—C24—C23 | 121.26 (15) |
| H131—C13—H132 | 109.1 | C25—C24—H24 | 119.4 |
| C17—C14—C13 | 100.98 (13) | C23—C24—H24 | 119.4 |
| C17—C14—C15 | 100.74 (14) | C24—C25—C26 | 121.81 (16) |
| C13—C14—C15 | 108.81 (14) | C24—C25—H25 | 119.1 |
| C17—C14—H14 | 114.9 | C26—C25—H25 | 119.1 |
| C13—C14—H14 | 114.9 | C21—C26—C25 | 115.72 (16) |
| C15—C14—H14 | 114.9 | C21—C26—H26 | 122.1 |
| C14—C15—C16 | 102.17 (13) | C25—C26—H26 | 122.1 |
| C12—O12—C10—O17 | -29.50 (19) | C14—C15—C16—C11 | 9.50 (18) |
| C12—O12—C10—O21 | -149.20 (12) | C10—O17—C17—C14 | -107.09 (15) |
| C12—O12—C10—O22 | 95.01 (15) | C10—O17—C17—C11 | -1.20 (18) |
| C17—O17—C10—O12 | 48.45 (18) | C13—C14—C17—O17 | 62.57 (16) |
| C17—O17—C10—O21 | 168.94 (11) | C15—C14—C17—O17 | 174.35 (12) |
| C17—O17—C10—O22 | -75.77 (15) | C13—C14—C17—C11 | -54.55 (15) |
| C21—O21—C10—O12 | -130.62 (13) | C15—C14—C17—C11 | 57.24 (14) |
| C21—O21—C10—O17 | 104.97 (13) | C12—C11—C17—O17 | -54.39 (16) |
| C21—O21—C10—O22 | -12.80 (15) | C16—C11—C17—O17 | -166.60 (13) |
| C22—O22—C10—O12 | 130.32 (13) | C12—C11—C17—C14 | 61.39 (14) |
| C22—O22—C10—O17 | -102.52 (14) | C16—C11—C17—C14 | -50.83 (15) |
| C22—O22—C10—O21 | 13.21 (15) | C10—O21—C21—C22 | 7.81 (17) |

supplementary materials

| | | | |
|-----------------|--------------|-----------------|--------------|
| C10—O12—C12—C11 | -34.36 (18) | C10—O21—C21—C26 | -173.44 (16) |
| C10—O12—C12—C13 | 78.75 (16) | C26—C21—C22—C23 | 0.2 (3) |
| C17—C11—C12—O12 | 72.75 (14) | O21—C21—C22—C23 | 179.04 (14) |
| C16—C11—C12—O12 | 178.71 (12) | C26—C21—C22—O22 | -178.16 (14) |
| C17—C11—C12—C13 | -45.31 (15) | O21—C21—C22—O22 | 0.67 (17) |
| C16—C11—C12—C13 | 60.65 (17) | C10—O22—C22—C23 | 173.13 (16) |
| O12—C12—C13—C14 | -104.89 (14) | C10—O22—C22—C21 | -8.63 (16) |
| C11—C12—C13—C14 | 11.96 (17) | C21—C22—C23—C24 | 0.0 (2) |
| C12—C13—C14—C17 | 26.56 (16) | O22—C22—C23—C24 | 178.00 (15) |
| C12—C13—C14—C15 | -78.90 (16) | C22—C23—C24—C25 | -0.1 (2) |
| C17—C14—C15—C16 | -42.05 (16) | C23—C24—C25—C26 | 0.1 (3) |
| C13—C14—C15—C16 | 63.58 (17) | C22—C21—C26—C25 | -0.2 (2) |
| C12—C11—C16—C15 | -75.92 (17) | O21—C21—C26—C25 | -178.81 (15) |
| C17—C11—C16—C15 | 25.97 (18) | C24—C25—C26—C21 | 0.0 (2) |

Fig. 1

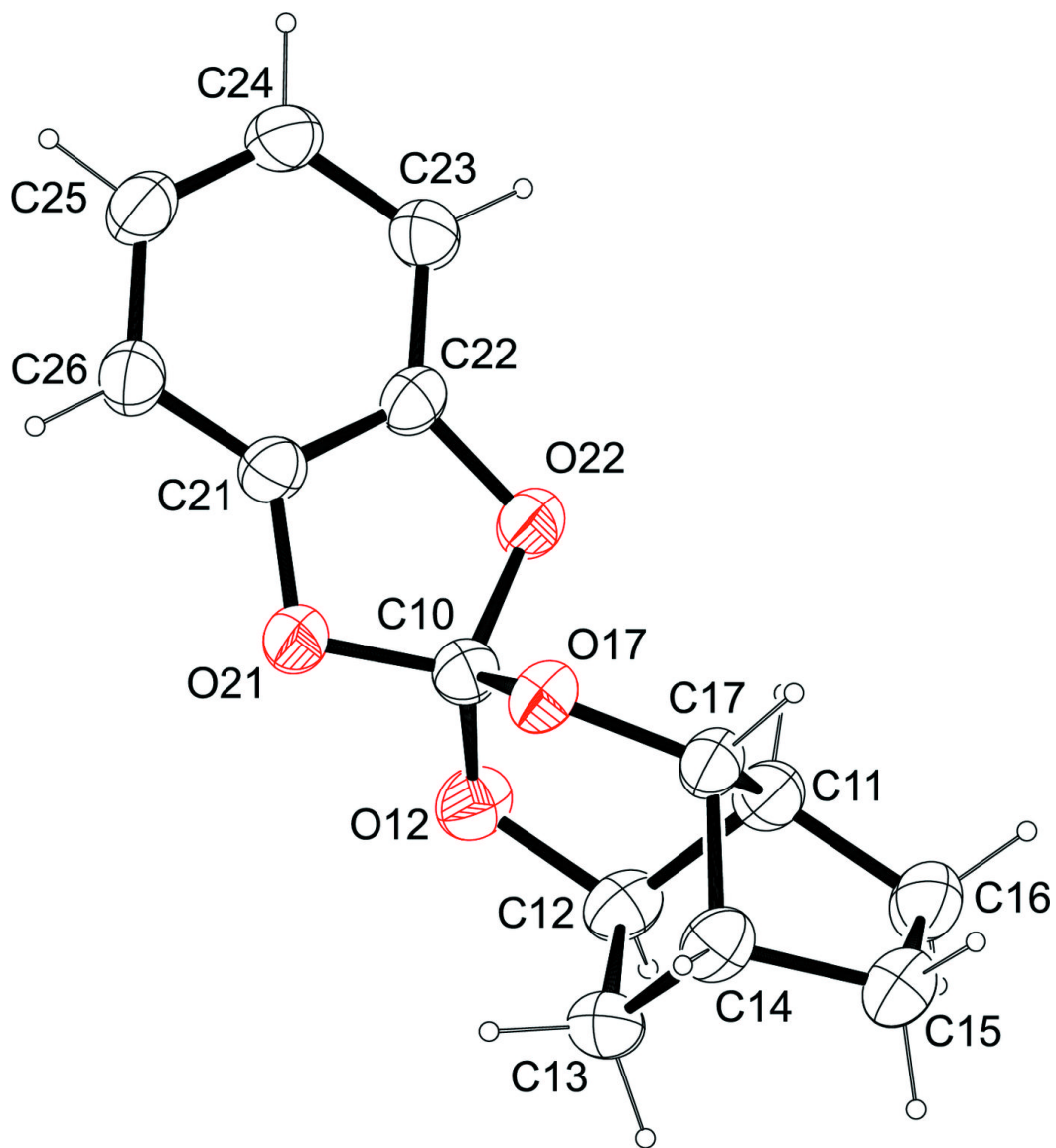


Fig. 2

